

SCS ENGINEERS

March 26, 2009
File No. 02200016.04

Mr. Steve Krajcsik
Anne Arundel County Dept. of Public Works
389 Burns Crossing Road
Severn, Maryland 21144-3411

Subject: 2008 Emission Certification Report and Air Toxics Certification
Millersville Landfill, Anne Arundel County, Maryland

Dear Steve:

SCS Engineers (SCS) has prepared the attached 2008 Emission Certification Report (ECR) and Air Toxics Certification (ATC) for the Millersville Landfill. Emissions from the landfill for many pollutants are based on the collection efficiency of the LFG system at the landfill, the pollutant destruction efficiency of the LFG flare, and the results of the flare emissions test.

Based on actual site measurements, a total of 98.1 percent of the estimated LFG generated at the landfill in 2008 was collected by the LFG system and delivered to the flare for combustion. Based on the results of stack testing of the flare in 1997, the destruction efficiency of the flare was measured to be 99.91 percent, greater than the 98 percent destruction efficiency required by the EPA's NSPS regulations.

The air pollutants to be certified are: filterable particulate matter with an aerodynamic diameters less than 10 micrometers (PM10) and less than 2.5 micrometers (PM2.5), filterable and condensable particulate matter, sulfur oxides (SOX), nitrogen oxides (NOX), carbon monoxide (CO), volatile organic compounds (VOCs), and hazardous air pollutants (HAPs). Additionally, greenhouse gas (GHG) air pollutants are to be reported. These include methane (CH4), carbon dioxide (CO2), nitrous oxide (N2), hydrofluorocarbons (HFCs), perfluorocarbons (PFCs) and sulfur hexafluoride (SF6); of these GHGs, only methane and carbon dioxide are typically found in LFG.

The following briefly describes the approach SCS used to estimate emissions of each of these pollutants from the Millersville Landfill.

- **PM** - Particulate matter is emitted from the combustion of LFG in the flare. Emission factors contained in U.S. EPA's Compilation of Air Pollutant Emission Factors (AP-42), as revised in November 1998, were used to estimate PM10 emissions from the flare.

Particulate matter is also emitted from the operation of equipment associated with landfill operations. For estimating these emissions, SCS utilized emission factors and guidelines provided in the U.S. EPA's Compilation of Air Pollutant Emission Factors (AP-42).

- **SO_x** - Sulfur oxides are formed when fuel that contains sulfur-bearing compounds (e.g.,



LFG) is combusted. The SO_x emissions were estimated from stack test results (for enclosed flare operation) and the actual records of LFG flow to the flare.

- **NO_x** - Nitrogen oxides are also a product of fuel combustion. NO_x emissions were estimated from stack test results (for enclosed flare operation) and the actual records of LFG flow to the flare.
- **CO** - Carbon monoxide results from incomplete combustion of LFG in the flare. As with SO_x and NO_x, CO emissions were estimated from stack test results (for enclosed flare operation) and the actual records of LFG flow to the flare.
- **VOCs** - VOCs are present in LFG, and they are emitted via passive release from the landfill surface and, in smaller quantities, as uncombusted VOCs from the flare. Total VOC emissions are a function of the total LFG generated at the site, the collection efficiency of the LFG collection system, and the flare destruction efficiency, 99.91 percent for the enclosed flare (stack test results).

VOCs are a subset (39 percent by volume according to the EPA's AP-42 Section 2-4) of non-methane organic compounds (NMOCs). The site NMOC concentration was updated during testing conducted in April 2004.

- **HAPs** - Some HAPs are present in LFG. SCS used results from laboratory analysis conducted in April 2004 and measured LFG collection and destruction efficiencies to estimate the emissions of HAPs other than hydrochloric acid (HCl) from landfill and the flare. SCS used stack test results and actual records of LFG flow to the flare to calculate emission of HCl, a HAP which is a product of combustion.
- **CO₂** - Carbon dioxide is emitted both as a component of raw LFG and as a result of the combustion of methane in the flare. The CO₂ emissions are a function of the total LFG generated at the site and the rate of methane capture and combustion in the flare.
- **CH₄** - Methane is emitted both as a component of raw LFG and as a result of uncombusted methane being exhausted by the flare (this fraction is typically very small). Methane emissions are a function of the total LFG generated at the site, the methane capture rate, and the destruction efficiency of the flare (99.91 percent).

In addition to the above-listed pollutants, the MDE requires the emission certification of 192 compounds considered to be air toxics. A number of the compounds considered by MDE to be air toxics are found in LFG and are emitted via passive release from the landfill surface and, in smaller quantities, as uncombusted compounds from the flare. SCS generally used results from laboratory analysis conducted in April 2004 and LFG collection and destruction efficiencies to estimate the emission of the various air toxic compounds present in LFG.

Table 1 presents a summary of the annual emissions for the landfill in 2008, given in both tons per year and pounds per day. Supporting calculations are included in the certification report.

Table 1. Millersville Landfill Emission Summary

Pollutant	2008 Emission (ton/yr)	2008 Emissions (lb/day)
VOCs	0.2	1.1
PM Condensable	1.4	7.4
PM Filterable	9.7	52.9
Sulfur Oxides	5.4	29.5
Oxides of Nitrogen	6.6	36.5
Carbon Monoxide	0.2	1.0
¹ Billable Air Toxics	0.1	0.5
¹ Total Air Toxics	0.1	0.7
Methane	134.1	734.4
Carbon Dioxide	36,815	201,726

¹ Emission statement includes emission for individual HAPs and air toxic compounds.

Two copies of the Emission Certification package should be sent by April 1 to MDE at the following address:

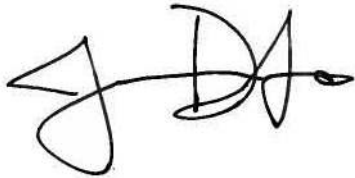
Attn: Laramie Daniel
Air Quality Compliance Program
Air and Radiation Management Administration
Maryland Department of the Environment
1800 Washington Boulevard, Suite 715
Baltimore, Maryland 21230-1720

In the transmittal to MDE, a statement should be included certifying the Landfill is in compliance with Maryland's Air Toxic Regulations (COMAR 26.11.15) for 2008.

If you have any questions regarding the report, please do not hesitate to contact any of the undersigned.

Very truly yours,

Mr. Stephen Krajcsik
March 26, 2009
Page 4

A handwritten signature in black ink, appearing to read 'J. Demko', with a stylized, cursive script.

Justina M. Demko
Associate Staff Professional
SCS ENGINEERS

A handwritten signature in black ink, appearing to read 'Joshua Roth', with a stylized, cursive script.

Joshua G. Roth, P.E.
Project Manager
SCS ENGINEERS

Enclosures

MARYLAND DEPARTMENT OF THE ENVIRONMENT
 1800 Washington Boulevard, Suite 715 • Baltimore Maryland 21230-1720
 (410) 537-3000 • 1-800-633-6101 • <http://www.mde.state.md.us>
 Air and radiation Management Administration
 Air Quality Compliance Program
 (410) 537-3220

FORM 1

GENERAL FACILITY INFORMATION
EMISSION CERTIFICATION REPORT

Report for Calendar Year: 2008

A. FACILITY IDENTIFICATION		--Do Not Write in This Space--	
Facility Name: MILLERSVILLE LANDFILL & RESOURCE RECOVERY FACILITY		Date Received Local	
Address 389 BURNS CROSSING ROAD		Date Received State	
City: SEVERN County: ANNE ARUNDEL Zip: 21144		AIRS Code	
B. Briefly describe the Major Function of the Premises		FINDS Code	
MUNICIPAL SOLID WASTE LANDFILL		SIC Code	
		Premise Number	
		Source Latitude and Longitude	
C. SEASONAL PRODUCTION (if applicable)		Reviewed Name	Date
Winter (Dec.-Feb.) ___	Spring (Mar.-May) ___	Summer (June-Aug.) ___	Fall (Sept.-Nov.) ___
D. Explain any Increase/Decrease From Previous Calendar Year for Each Registration at this premises.			
E. CONTROL DEVICE INFORMATION (for NOx and VOC sources only)			
Control Device	Capture Efficiency	Removal Efficiency	
LANDFILL GAS CONTROL SYSTEM	98.11%	-	
ENCLOSED GROUND FLARE	-	99.91%	
I am familiar with the premises and the installation and sources for which this report is submitted. I have personally examined the information in this report, which consists of 26 pages (including attachments), and certify that the information is correct to the best of my knowledge.			
Stephen J. Kracjsick PE.		Disposal Maintenance Manager	
Name(Print/Type)		Title	
		3/24/2009	
		Date	
_____		410-222-6108	
Signature		Telephone Number	

FORM 2

**CRITERIA AIR POLLUTANTS
EMISSIONS CERTIFICATION REPORT**

Facility Name: MILLERSVILLE LANDFILL & RESOURCE RECOVERY FACILITY

Facility ID#: 003-0086

Calendar Year: 2008

Pollutant: VOCs

Equipment Description/ Registration No	SCC Number	Fuel		Actual Emissions		Operating Schedule (Actual)				TOSD	Operating Schedule			Emissions Methods
				Tons/yr	Lbs/day	Hrs/day	Days/week	Week/yr	Days/yr	Lbs/day	Hrs/day	Start	End	
Landfill 16-1862		N/A	S	-	-	24	7	52	366	-	24			
			F	0.2	1.0					1.0				
Landfill Gas Flare System 16-0658		N/A	S	0.0	0.0	24	7	52	366	0	24			C1
			F	-	-					-				
Grinder		Diesel	S	0.0	0.1	1	6	52	312	0.1	1			C3
			F	-	-					-				
Total				0.2	1.1					1.1				

S-Stack Emissions

F-Fugitive

Daily emissions (lbs/day) are lbs/operating day of the source

TOSD-Typical Ozone Season Day means a typical day of that period of the year during which conditions for photochemical conditions are most favorable, which is generally during sustained periods of direct sunlight and warm temperatures (April-September). This section needs to be completed only for VOC and NOx sources.

Fuel: Include emissions for each fuel used. If more than one fuel is used, calculate and list emissions separately for each fuel.

Emission Estimation Method

- A1-U.S. EPA Reference Method
- A2-Other Particulate Sampling Train
- A3-Liquid Absorption Technique
- A4-Solid Absorption Technique
- A5-Frezing Out Technique
- A9-Other, Specify

- C1-User calculated based on source test or other measurement
- C2-User calculated based on material balance using engineering knowledge of the process
- C3-User calculated based on AP-42
- C4-User calculated by best guess/engineering judgment

- C5-User calculated based on a State or local agency emission factor
- C6-New construction, not operational
- C7-Source closed, operation ceased
- C8-Computer calculated based on standard

FORM 2

**CRITERIA AIR POLLUTANTS
EMISSIONS CERTIFICATION REPORT**

Facility Name: MILLERSVILLE LANDFILL & RESOURCE RECOVERY FACILITY

Facility ID#: 003-0086

Calendar Year: 2008

Pollutant: NO_x

Equipment Description/ Registration No	SCC Number	Fuel		Actual Emissions		Operating Schedule (Actual)				TOSD	Operating Schedule		Emissions Methods	
				Tons/yr	Lbs/day	Hrs/day	Days/week	Week/yr	Days/yr	Lbs/day	Hrs/day	Start		End
Landfill 16-1862		N/A	S	0.00	0.00	24	7	52	366	0.00	24			C2
			F	-	-					-				
Landfill Gas Flare System 16-0658		N/A	S	3.0	16.6	24	7	52	366	16.6	24			C1
			F	-	-					-				
Grinder		Diesel	S	3.6	19.9	1	6	52	312	19.9	1			C1
			F											
Total				6.6	36.5					36.5				

S-Stack Emissions

F-Fugitive

Daily emissions (lbs/day) are lbs/operating day of the source

TOSD-Typical Ozone Season Day means a typical day of that period of the year during which conditions for photochemical conditions are most favorable, which is generally during sustained periods of direct sunlight and warm temperatures (April-September). This section needs to be completed only for VOC and NO_x sources.

Fuel: Include emissions for each fuel used. If more than one fuel is used, calculate and list emissions separately for each fuel.

Emission Estimation Method

- A1-U.S. EPA Reference Method
- A2-Other Particulate Sampling Train
- A3-Liquid Absorption Technique
- A4-Solid Absorption Technique
- A5-Frezing Out Technique
- A9-Other, Specify

- C1-User calculated based on source test or other measurement
- C2-User calculated based on material balance using engineering knowledge of the process
- C3-User calculated based on AP-42
- C4-User calculated by best guess/engineering judgment

- C5-User calculated based on a State or local agency emission factor
- C6-New construction, not operational
- C7-Source closed, operation ceased
- C8-Computer calculated based on standard

FORM 2

**CRITERIA AIR POLLUTANTS
EMISSIONS CERTIFICATION REPORT**

Facility Name: MILLERSVILLE LANDFILL & RESOURCE RECOVERY FACILITY

Facility ID#: 003-0086

Calendar Year: 2008

Pollutant: SO_x

Equipment Description/ Registration No	SCC Number	Fuel		Actual Emissions		Operating Schedule (Actual)				TOSD	Operating Schedule			Emissions Methods
				Tons/yr	Lbs/day	Hrs/day	Days/week	Week/yr	Days/yr	Lbs/day	Hrs/day	Start	End	
Landfill 16-1862		N/A	S	N/A	N/A	24	7	52	366	N/A	24			C2
			F	-	-									
Landfill Gas Flare System 16-0658		N/A	S	5.3	28.8	24	7	52	366	28.8	24			C1
			F	-	-					-				
Grinder		Diesel	S	0.1	0.7	1	6	52	312	0.7	1			C3
			F	-	-									
Total				5.4	29.5					29.5				

S-Stack Emissions

F-Fugitive

Daily emissions (lbs/day) are lbs/operating day of the source

TOSD-Typical Ozone Season Day means a typical day of that period of the year during which conditions for photochemical conditions are most favorable, which is generally during sustained periods of direct sunlight and warm temperatures (April-September). This section needs to be completed only for VOC and NO_x sources.

Fuel: Include emissions for each fuel used. If more than one fuel is used, calculate and list emissions separately for each fuel.

Emission Estimation Method

- A1-U.S. EPA Reference Method
- A2-Other Particulate Sampling Train
- A3-Liquid Absorption Technique
- A4-Solid Absorption Technique
- A5-Frezing Out Technique
- A9-Other, Specify

- C1-User calculated based on source test or other measurement
- C2-User calculated based on material balance using engineering knowledge of the process
- C3-User calculated based on AP-42
- C4-User calculated by best guess/engineering judgment

- C5-User calculated based on a State or local agency emission factor
- C6-New construction, not operational
- C7-Source closed, operation ceased
- C8-Computer calculated based on standard

FORM 2

**CRITERIA AIR POLLUTANTS
EMISSIONS CERTIFICATION REPORT**

Facility Name: MILLERSVILLE LANDFILL & RESOURCE RECOVERY FACILITY

Facility ID#: 003-0086

Calendar Year: 2008

Pollutant: CO

Equipment Description/ Registration No	SCC Number	Fuel		Actual Emissions		Operating Schedule (Actual)				TOSD	Operating Schedule			Emissions Methods
				Tons/yr	Lbs/day	Hrs/day	Days/week	Week/yr	Days/yr	Lbs/day	Hrs/day	Start	End	
Landfill 16-1862		N/A	S	N/A	N/A	24	7	52	366	N/A	24			
			F	-	-					-				
Landfill Gas Flare System 16-0658		N/A	S	0	0.2	24	7	52	366	0.2	24			C1
			F	-	-					-				
Grinder		Diesel	S	0.2	1.0	1	6	52	312	1.0	1			C1
			F	-	-					-				
Total				0.2	1.2					1.2				

S-Stack Emissions

F-Fugitive

Daily emissions (lbs/day) are lbs/operating day of the source

TOSD-Typical Ozone Season Day means a typical day of that period of the year during which conditions for photochemical conditions are most favorable, which is generally during sustained periods of direct sunlight and warm temperatures (April-September). This section needs to be completed only for VOC and NOx sources.

Fuel: Include emissions for each fuel used. If more than one fuel is used, calculate and list emissions separately for each fuel.

Emission Estimation Method

- A1-U.S. EPA Reference Method
- A2-Other Particulate Sampling Train
- A3-Liquid Absorption Technique
- A4-Solid Absorption Technique
- A5-Frezing Out Technique
- A9-Other, Specify

- C1-User calculated based on source test or other measurement
- C2-User calculated based on material balance using engineering knowledge of the process
- C3-User calculated based on AP-42
- C4-User calculated by best guess/engineering judgment

- C5-User calculated based on a State or local agency emission factor
- C6-New construction, not operational
- C7-Source closed, operation ceased
- C8-Computer calculated based on standard

FORM 3: PM_{total}

**EMISSIONS CERTIFICATION REPORT
Particulate Matter – Total**

Facility Name: MILLERSVILLE LANDFILL & RESOURCE RECOVERY FACILITY

Facility ID#: 003-0086

Calendar Year: 2008

Pollutant: PM_{total}*

Equipment Description/ Registration No	SCC Number	Fuel		PM – Filterable		PM ₁₀ – Filterable		PM _{2.5} – Filterable		PM – Condensable		Operation (days/yr)	Emissions Methods
				Tons/yr	Lbs/day	Tons/y	Lbs/day	Tons/yr	Lbs/day	Tons/yr	Lbs/day		
Landfill 16-1862			S	-	-	-	-	-	-	-	-	366	C2,C3
			F	8.3	45.5	8.3	45.5	2.8	15.3	0.0	0.0		
Landfill Gas Flare System16-0658		Landfill gas	S	1.4	7.4	1.4	7.4	1.4	7.4	1.4	7.4	366	C2, C3
			F	-	-	-	-	-	-	-	-		
Grinder		Diesel	S	0.0	0.2	0.0	0.2	0.0	0.2	0.0	0.0	312	C1
			F	-	-	-	-	-	-	-	-		
Total				9.7	52.9	9.7	52.9	4.2	22.7	1.4	7.4		

S-Stack Emissions

F-Fugitive

Daily emissions (lbs/day) are lbs/operating day of the source

Fuel: Include emissions for each fuel used. If more than one fuel is used, calculate and list emissions separately for each fuel.

Emission Estimation Method

- A1-U.S. EPA Reference Method
- A2-Other Particulate Sampling Train
- A3-Liquid Absorption Technique
- A4-Solid Absorption Technique
- A5-Frezing Out Technique
- A9-Other, Specify

- C1-User calculated based on source test or other measurement
- C2-User calculated based on material balance using engineering knowledge of the process
- C3-User calculated based on AP-42
- C4-User calculated by best guess/engineering judgment

FORM 4

Calendar Year: 2008

TOXIC AIR POLLUTANTS
EMISSIONS CERTIFICATION REPORT

Facility Name: MILLERSVILLE LANDFILL & RESOURCE RECOVERY FACILITYFacility ID# .003-0086Pollutant: Hydrochloric acid *:

Equipment Description / Registration Number		Actual Emissions		Control Device**	% Efficiency
		Lbs/hr	Tons/yr		
MSW Landfill (16-1862)	Stack				
	Fugitive			O	
LFG Flare System (16-0658)	Stack	0.0	0.1		
	Fugitive				
	Stack				
	Fugitive				
	Stack				
	Fugitive				
	Stack				
	Fugitive				
	Stack				
	Fugitive				
Total		0.0	0.1		

* Please attach all calculations.

* See Attachment 1 for the minimum reporting values.

**Control Device:

S = Scrubber
 B = Baghouse
 ESP = Electrostatic
 Precipitator
 A = Afterburner
 C = Condenser
 AD = Adsorbtion
 O = Other

¹ Emissions must be broken down by equipment registration number (ex. 9-0076, 9-0077)

FORM 5

BILLABLE TOXIC AIR POLLUTANTS
EMISSIONS CERTIFICATION REPORT

Calendar Year: **2008**Facility Name: MILLERSVILLE LANDFILL & RESOURCE RECOVERY FACILITYFacility ID#: 003-0086

Chemical Name	CAS Number		Actual Emissions		Estimation Method
			Tons/yr	Lbs/day	
Methyl Chloroform	71-55-6	S	0	0.00	C2
		F	0	0.00	C2
Carbon Disulfide	75-15-0	S	0	0.00	C2
		F	0	0.00	C2
Carbonyl Sulfide	463-58-1	S	0	0.00	C2
		F	0	0.00	C2
Methylene Chloride	75-09-2	S	0	0.00	C2
		F	0	0.00	C2
Perchloroethylene	127-18-4	S	0	0.00	C2
		F	0	0.00	C1
Hydrochloric Acid	7647-01-0	S	0.1	0.7	C1
		F	0.0	0.0	C2
Chlorine	7782-50-5	S	0.0	0.00	C2
		F	0.0	0.00	C2
Cyanide Compounds	57-12-5	S	0.0	0.00	C3
		F	0.0	0.00	C3
Hydrogen Fluoride	7664-39-3	S	0.0	0.00	C3
		F	0.0	0.00	C3
Phosphine	7803-51-2	S	0.00	0.00	C3
		F	0.00	0.00	C3
Titanium Tetrachloride	7550-45-0	S	0.0	0.00	C3
		F	0.0	0.00	C3
TOTALS			0.1	0.7	

Emission Estimation Method

A1-U.S. EPA Reference Method

A2-Other Particulate Sampling Train

A3-Liquid Absorption Technique

A4-Solid Absorption Technique

A5-Frezing Out Technique

A9-Other, Specify

C1-User calculated based on source test or other measurement

C2-User calculated based on material balance using engineering knowledge of the process

C3-User calculated based on AP-42

C4-User calculated by best guess/engineering judgment

C5-User calculated based on a State or local agency emission factor

C6-New construction, not operational

C7-Source closed, operation ceased

C8-Computer calculated based on standard

This form to include only the eleven chemicals identified

n/a - not applicable

S - Stack Emissions

F - Fugitive Emissions

Daily emissions (lbs/day) are lbs/operating day of the source

PLEASE NOTE: Be sure to attach all data and calculations necessary to support the emissions figures shown above.

Actual Emissions reported to the minimum reporting values specified by the MDE Attachment 1

FORM 6:Greenhouse GasesCalendar Year: 2008**GREENHOUSE GAS AIR POLLUTANTS**
EMISSIONS CERTIFICATION REPORTFacility Name: MILLERSVILLE LANDFILL & RESOURCE RECOVERY FACILITYFacility ID# .003-0086Pollutant: Carbon dioxide (CO₂)*

Equipment Description / Registration Number		Actual Emissions		
		Tons/yr	Lbs/day	Lbs/hr
MSW Landfill (16-1862)	Stack	-	-	-
	Fugitive	18,583	101,824	4,242
LFG Flare System (16-0658)	Stack	18,232	99,901	4,162
	Fugitive	-	-	-
	Stack			
	Fugitive			
	Stack			
	Fugitive			
	Stack			
	Fugitive			
	Stack			
	Fugitive			
	Stack			
	Fugitive			
Total		36,815	201,725	8,404

This form must be used to report
Greenhouse gas emissions:

- carbon dioxide (CO₂)
- methane (CH₄)
- nitrous oxide (N₂O)
- hydrofluorocarbons (HFCs)
- perfluorocarbons (PFCs)
- sulfur hexafluoride (SF₆)

* Use a separate form for each
pollutant.

* Please attach all calculations.

¹ Emissions must be broken down by equipment registration number (ex. 9-0076, 9-0077)

FORM 6:Greenhouse Gases

Calendar Year: 2008

GREENHOUSE GAS AIR POLLUTANTS
EMISSIONS CERTIFICATION REPORT

Facility Name: MILLERSVILLE LANDFILL & RESOURCE RECOVERY FACILITY
 Pollutant: Methane (CH₄)*

Facility ID# .003-0086

Equipment Description / Registration Number		Actual Emissions		
		Tons/yr	Lbs/day	Lbs/hr
MSW Landfill (16-1862)	Stack	-	-	-
	Fugitive	128	701	29.2
LFG Flare System (16-0658)	Stack	6.0	32.7	1.4
	Fugitive	-	-	-
	Stack			
	Fugitive			
	Stack			
	Fugitive			
	Stack			
	Fugitive			
	Stack			
	Fugitive			
	Stack			
	Fugitive			
Total		134.1	734.4	30.6

This form must be used to report Greenhouse gas emissions:

- carbon dioxide (CO₂)
- methane (CH₄)
- nitrous oxide (N₂O)
- hydrofluorocarbons (HFCs)
- perfluorocarbons (PFCs)
- sulfur hexafluoride (SF₆)

* Use a separate form for each pollutant.

* Please attach all calculations.

¹ Emissions must be broken down by equipment registration number (ex. 9-0076, 9-0077)

ATTACHMENT
(EMISSION CALCULATIONS)

**2008 Emissions Calculations
Millersville Landfill and
Resource Recovery Facility**

Calculated by: J. M. Demko
Checked by: J.G. Roth

PART 1 - LANDFILL GAS EMISSIONS

The following parameters and values are utilized in these computations:

1. Site specific methane content =	52.2%	[AACo personnel provided data]
2. Site specific LFG flow rate =	1,185.0	cfm [AACo personnel provided data]
3. Site specific methane flow rate =	618.6	cfm
4. Normalized LFG flow rate =	1,237.1	cfm (@ 50 percent methane)
5. Methane generation rate =	630.5	cfm
6. Methane generation rate (metric)	9,384,987.5	m ³ /yr
6. LFG generation rate (@ 50 % CH ₄)=	1,261	cfm [see Table 2]
7. VOC generation rate =	9.9	tons [see Table 2]
8. Flare control efficiency =	99.91%	[1997 Source Test]
9. Site specific NMOC conc. =	343.3	ppmv (site specific testing in July 2003)
10. VOC concentration =	39%	of NMOC concentration (per AP-42)

Step 1. Calculate Average Site-Specific LFG Heat (BTU) Content

Using the standard heating value for LFG of 500 BTU/ft³ (at 50 percent methane content) and the HHV of methane the site-specific LFG heating value is:

$$= (\text{site specific methane content} / 50\% \text{ methane}) * (500 \text{ BTU/ft}^3)$$

$$= \mathbf{522.0 \text{ BTU/ft}^3 \text{ LFG}}$$

where:

$$\text{methane content} = 52.2\%$$

Step 2. Compute the Site-Specific NO_x Emissions

The emission of NO_x from the enclosed ground flare is estimated using the site-specific emissions testing results from the "Source Emissions Test Report" by Kilkelly Environmental Associates (Sept. 1997).

Using the emissions testing result of 0.69 lb NO_x per hour of operation, the emission from the enclosed flare is:

$$= [(0.69 \text{ lb NO}_x \text{ per hour operation}) * (8,760 \text{ hours operation}) * (1 \text{ ton}/2,000 \text{ lbs})]$$

$$= \mathbf{3.0 \text{ tons NO}_x \text{ from enclosed flare operation}}$$

$$= 16.6 \text{ lbs/day NO}_x \text{ from enclosed flare operation}$$

**2008 Emissions Calculations
Millersville Landfill and
Resource Recovery Facility**

Calculated by: J. M. Demko
Checked by: J.G. Roth

Step 3. Compute the Site-Specific CO Emissions

The emission of CO from the enclosed ground flare is estimated using the site-specific emissions testing results from the "Source Emissions Test Report" by Kilkelly Environmental Associates (Sept. 1997).

Using the emissions testing result of 0.01 lb CO per hour of operation, the emission from the enclosed flare is:

$$= [(0.01 \text{ lb CO per hour operation}) * (8,760 \text{ hours operation}) * (1 \text{ ton}/2,000 \text{ lbs})]$$

$$=$$

$$= \quad \quad \quad \mathbf{0.0 \text{ tons CO from enclosed flare operation}}$$

$$= \quad \quad \quad 0.2 \text{ lbs/day CO from enclosed flare operation}$$

Step 4. PM10 Emissions

Site-specific data for the emission of PM10 and PM2.5 from the enclosed ground flare is not available. Therefore, the emission of PM10 and PM2.5 is estimated using the EPA AP-42 emission factor for PM10 of 17 lb PM10 per 1,000,000 cubic feet of methane combusted.

*EPA does not distinguish between PM10 and PM2.5 emissions, though EPA does suggest that, for LFG particulate flare emissions, PM10 and PM2.5 are equivalent.

*EPA does not provide emission factors for condensable and filterable PM fractions. Thus, for purposes of this estimate, assume that 50 percent of the PM is filterable and 50 percent is condensable.

Using the total methane flow rate for Jan-Dec, the PM10 (and PM2.5) emissions are:

$$\text{LFG Throughput for 2008} = \quad \quad \quad 614,316,670 \text{ cf [AACo personnel provided data]}$$

$$(17 \text{ lb PM10 per } 10^6 \text{ cubic feet methane}) * (\text{total LFG flow (Jan-Dec), cf}) * (1 \text{ ton}/2,000 \text{ lbs}) * (\text{Site-specific methane content, \%})$$

$$= \quad \quad \quad 2.7 \text{ tons PM (filterable and condensable) total flare emissions}$$

$$\text{PM10 and PM2.5 Filterable} = \quad (2.7 \text{ tons PM10 and PM2.5 total flare emissions}) * (50\% \text{ estimated filterable})$$

$$= \quad \quad \quad \mathbf{1.35 \text{ tons PM10 and PM2.5 Filterable Emissions}}$$

$$\quad \quad \quad 7.39 \text{ lbs/day PM10 and PM2.5 Filterable Emissions}$$

$$\text{PM Condensable} = \quad (2.7 \text{ tons total PM flare emissions}) * (50\% \text{ estimated condensable})$$

$$= \quad \quad \quad \mathbf{1.35 \text{ tons PM Condensable Emissions}}$$

$$\quad \quad \quad 7.39 \text{ lbs/day PM Condensable Emissions}$$

Step 5. SOx Emissions

The emission of SOx from the enclosed ground flare is estimated using the site-specific emissions testing results from the "Source Emissions Test Report" by Kilkelly Environmental Associates (Sept. 1997).

Using the emissions testing result of 1.2 lb SOx per hour of operation, the emission from the enclosed flare is:

$$= [(1.2 \text{ lb SOx per hour operation}) * (8,760 \text{ hours operation}) * (1 \text{ ton}/2,000 \text{ lbs})]$$

$$=$$

$$= \quad \quad \quad \mathbf{5.3 \text{ tons SOx from enclosed flare operation}}$$

$$= \quad \quad \quad 28.8 \text{ lbs/day SOx from enclosed flare operation}$$

**2008 Emissions Calculations
Millersville Landfill and
Resource Recovery Facility**

Calculated by: J. M. Demko
Checked by: J.G. Roth

Step 6. VOC Emissions

The emission of VOCs from the flare and from the landfill (as a fugitive emission) is estimated using the LFG collection efficiency and the landfill's VOC generation rate (see attached Table 2 with LFG Modeling Results).

First, estimate the collection efficiency of the LFG collection system using the methane flow to the flare and the methane generation rate

$$= (\text{site specific methane flow, cfm}) / (\text{methane generation rate, cfm}) * 100$$

$$= 98.11\% \text{ collection efficiency}$$

where:

$$\begin{aligned} \text{methane generation rate} &= 630.5 \\ \text{site specific methane flow} &= 618.6 \end{aligned}$$

Next, calculate the uncombusted flare emission of VOCs (to the nearest 0.1 ton)

$$= (\text{VOC generation rate, tons}) * (\text{collection efficiency}) * (1 - \text{flare control efficiency})$$

$$= \mathbf{0.0 \text{ tons VOC total flare emissions}}$$

$$= 0.0 \text{ lbs/day VOC total flare emissions}$$

where:

$$\begin{aligned} \text{VOC generation rate (tons)} &= 9.9 \\ \text{collection efficiency} &= 98.1\% \\ \text{flare control efficiency} &= 99.9\% \end{aligned}$$

Next, calculate the uncollected landfill emission of VOCs (fugitive emissions)

$$= (\text{VOC generation rate, tons}) * (1 - \text{collection efficiency})$$

$$= \mathbf{0.2 \text{ tons VOC fugitive landfill emissions}}$$

$$= 1.0 \text{ lbs/day VOC fugitive landfill emissions}$$

where:

$$\begin{aligned} \text{VOC generation rate} &= 9.9 \\ \text{collection efficiency} &= 98.1\% \end{aligned}$$

**2008 Emissions Calculations
Millersville Landfill and
Resource Recovery Facility**

Calculated by: J. M. Demko
Checked by: J.G. Roth

Step 7. Toxic Air Pollutant (TAP) and Hazardous Air Pollutant (HAP) Emissions

The emission of toxic air pollutants (TAPs) from the flare and from the landfill (as a fugitive emission) is estimated using the LFG collection efficiency, the LFG generation rate, and the concentration of the pollutants, which are based upon site-specific test data.

The attached Table 3 present a summary of the landfill and flare emissions for the TAPs and HAPs respectively. The following is a sample calculation for the emission of Toluene - the emission of the other TAPs was completed in a similar manner, unless otherwise noted.

First, calculate the toluene volumetric flow rate using AP-42 equation 2.4(3)

$$\begin{aligned} & * \text{ The site-specific concentration for toluene is 31.6 ppm (31,600 ppb).} \\ & = (\text{LFG generation rate}) * (31.6 \text{ ppm}) / (1,000,000) * (1 \text{ m}^3/35.3 \text{ ft}^3) * (525,600 \text{ min/yr}) \\ & = \qquad \qquad \qquad 593.3 \text{ m}^3 \text{ toluene/yr} \end{aligned}$$

where:

LFG generation rate is converted from cfm to cubic meters per year
LFG generation rate (cfm) = 1,261

Next, calculate the mass flow of toluene generated using AP-42 equation 2.4(4)

$$\begin{aligned} & = [(\text{toluene volume flow}) * (92.13 \text{ g/mol})] / [(8.205 \times 10^{-5}) * (1000 \text{ g/kg}) * (298 \text{ K})] \\ & = \qquad \qquad \qquad 2,235.6 \text{ kg toluene/yr} \end{aligned}$$

where:

92.13 g/gmol is the molecular weight of toluene
8.205x10⁻⁵ is the ideal gas conversion factor
298 K is the assumed temperature of the LFG (equivalent to 25 deg C)
toluene volume flow (m³/yr) = 593.3

Next, calculate the uncombusted flare emission of toluene

$$\begin{aligned} & = (\text{toluene mass generation rate, kg}) * (\text{collection efficiency}) * (1 - \text{flare control efficiency}) * (1 \text{ ton}/909 \text{ kg}) \\ & = \qquad \qquad \qquad \mathbf{0.0 \text{ tons toluene flare emissions}} \end{aligned}$$

where:

toluene mass generation (kg) = 2,235.6
normalized collection efficiency = 98.1%
flare control efficiency = 99.9%

**2008 Emissions Calculations
Millersville Landfill and
Resource Recovery Facility**

Calculated by: J. M. Demko
Checked by: J.G. Roth

Finally, calculate the uncollected landfill emission of toluene (fugitive emissions)

$$= (\text{toluene mass generation rate, kg}) * (1 - \text{normalized collection efficiency}) * (1 \text{ ton}/909 \text{ kg})$$

$$= \quad \quad \quad \mathbf{0.0 \text{ tons toluene fugitive landfill emissions}}$$

where:

$$\text{toluene mass generation (kg)} = 2,235.6$$

$$\text{normalized collection efficiency} = 98.1\%$$

Step 8. Calculate the Site-Specific CH₄ Emissions

First, estimate the collection efficiency of the LFG collection system using the methane flow to the flare and the methane generation rate

$$= (\text{site specific methane flow, cfm}) / (\text{methane generation rate, cfm}) * 100$$

$$= \quad \quad \quad 98.11\% \text{ collection efficiency}$$

where:

$$\text{methane generation rate} = 630.5$$

$$\text{site specific methane flow} = 618.6$$

Then using the metric methane generation rate and the Ideal Gas Law,

$$(\text{LFG generation rate, cubic meter/yr}) * (\text{MW of CH}_4, \text{ g/mol}) * (\text{Pressure, Pa}) / (\text{R, m}^3\text{-Pa/gmol-K}) * (1000\text{g}/1\text{kg}) * (273 + \text{T, K})$$

$$= \quad \quad \quad 6,139,554.2 \text{ kg/year CH}_4$$

where:

Pressure = 101,300	Pa
Molecular Weight of CH ₄ = 16	grams/mol
Temperature = 25	Celsius
Ideal gas conversion factor, R = 8.314	m ³ -Pa/gmol-K

Next, multiply mass flow rate of methane by normalized collection efficiency

$$= (\text{Mass flow rate, kg/yr}) * (1 - \text{Collection efficiency, \%}) * (1000\text{g}/1\text{kg}) * (1 \text{ lbs}/453.6\text{g}) * (1 \text{ ton}/2000\text{lbs})$$

$$= \quad \quad \quad \mathbf{128.1 \text{ tons CH}_4 \text{ fugitive emissions from the Landfill}}$$

$$\quad \quad \quad 701.7 \text{ lbs/day}$$

$$\quad \quad \quad 29.2 \text{ lbs/hr}$$

**2008 Emissions Calculations
Millersville Landfill and
Resource Recovery Facility**

Calculated by: J. M. Demko
Checked by: J.G. Roth

Finally, calculate the uncombusted flare emission of methane

$$= (\text{Mass flow rate, kg/yr}) * (\text{collection efficiency}) * (1 - \text{flare control efficiency}) * (1 \text{ ton}/909 \text{ kg})$$

$$= \begin{array}{l} \mathbf{6.0 \text{ tons CH}_4 \text{ flare emissions}} \\ 32.7 \text{ lbs/day} \\ 1.4 \text{ lbs/hr} \end{array}$$

where:

$$\text{mass flow rate (kg)} = 6,139,554.2$$

$$\text{normalized collection efficiency} = 98.1\%$$

$$\text{flare control efficiency} = 99.9\%$$

Step 9. Calculate the Site-Specific CO2 Emissions

The CO2 emissions from the landfill gas are from the following:

- CO2 comprises approximately 50 percent of LFG generated. This CO2 is emitted to the atmosphere either as a fugitive (uncollected LFG) emission, or through the stack (as CO2 in LFG is "passed through" and uncombusted).
- CO2 is formed by the combustion of methane. All methane combusted in the flare is assumed to be converted to, and emitted as, CO2.

CO2 emission are, thus, estimated as follows:

CO2 contained in raw LFG

$$\text{CO}_2 \text{ generation rate} = (\text{LFG Generation Rate}) * (0.5, \text{ assumed } 50\% \text{ CO}_2 \text{ content of raw LFG})$$

$$= 630.5 \text{ cfm}$$

$$\begin{aligned} \text{CO}_2 \text{ in raw LFG} &= (\text{CO}_2 \text{ gen rate}) * (\text{CO}_2 \text{ molecular wt}) / (\text{universal gas constant}) * \\ & \quad (\text{gas temperature}) * (525,600 \text{ min}/1 \text{ yr}) * (1 \text{ kg}/1000 \text{ g}) * (2.2 \text{ lb}/1 \text{ kg}) * \\ & \quad (1 \text{ ton}/2000 \text{ lb}) * (35.31 \text{ ft}^3/1 \text{ m}^3) \end{aligned}$$

$$= 18,583 \text{ tons of CO}_2 \text{ from raw LFG}$$

CO2 formed in the flare by the combustion of methane

$$\begin{aligned} \text{Combustion of CH}_4 \text{ in Flare} &= (\text{Site Specific CH}_4 \text{ Flow Rate}) * (\text{CO}_2 \text{ molecular mass}) / (\text{universal gas constant}) * \\ & \quad (\text{gas temperature}) * (525,600 \text{ min}/1 \text{ yr}) * (1 \text{ kg}/1000 \text{ g}) * (2.2 \text{ lb}/1 \text{ kg}) * \\ & \quad (1 \text{ ton}/2000 \text{ lb}) * (35.31 \text{ ft}^3/1 \text{ m}^3) \end{aligned}$$

$$= 18,232 \text{ tons of CO}_2 \text{ from methane combustion}$$

Total CO2 Emissions:

CO2 in raw LFG emissions + CO2 from methane combustion emissions

$$= \begin{array}{l} \mathbf{36,815 \text{ tons of CO}_2 \text{ landfill emissions (combined flare and fugitive)}} \\ 201,726 \text{ lbs/day} \\ 8,405 \text{ lbs/hr} \end{array}$$

where:

$$\text{CO}_2 \text{ Molecular Mass} = 44.01 \text{ g/mol}$$

$$\text{Universal Gas Constant} = 0.00008205 \text{ cm-atm/gmol-k}$$

$$\text{Landfill Gas Temperature} = 298 \text{ K}$$

PART 2 - 1,000-HP HORIZONTAL GRINDER ENGINE EMISSIONS

Given

<u>Compound</u>	<u>Emission Factor</u>	<u>Source</u>
NOx	15 lb/hr	Manufacturer
CO	0.79 lb/hr	Manufacturer
SOx	0.303 lb/MMBtu	AP-42, Section 3.4 ²
PM10 Filterable	0.15 lb/hr	Manufacturer ³
VOC	0.08 lb/hr	Manufacturer ⁴
CO2	1,273.3 lb/hr	Manufacturer
PM2.5 Filterable	0.15 lb/hr	Manufacturer ³
Fuel Consumption	5,602.70 gal/yr	[data provided by landfill]
Fuel Heating value	142,000 Btu/gal	
Hours of operation	485.00 hrs/yr	[data provided by landfill]

Notes:

- 1) Where available, manufacturer emission factors were used. To be conservative, it was assumed that the engine operated at 100 percent load.
- 2) SOx emission rate based on a maximum sulfur content of diesel of 0.3 (as limited in permit).
- 3) The manufacturer provides an estimate for PM only. Assume this is equal to both PM10 and PM2.5, and that this represents the filterable PM10 and PM2.5 emission rate.
- 4) VOC is assumed to be equal to total Total Hydrocarbons provided by manufacturer.
- 5) Hazardous air pollutant emissions for the engine are provided in the attached Table 4.
- 6) Lb/day and Lb/hour emission rates are based on the whole year (365 days, and 8,760 hours per year).

Sample calculation

Tons/year

= (Emission factor, lb/hr) * (Hours of operation during the year) * (1 ton/2000lbs)

<u>Results</u>	<u>Emission</u>		
	[tpy]	[lbs/day]	[lbs/hr]
NOx	3.6	19.9	0.8
CO	0.2	1.0	0.0
SOx	0.1	0.7	0.0
PM10 Filterable	0.0	0.2	0.0
VOC	0.0	0.1	0.0
CO2	308.8	1691.9	70.5
PM2.5 Filterable	0.0	0.2	0.0

PART 3 - LANDFILL OPERATION PM EMISSIONS

A. Estimate of PM10 (dust) emissions from active working face filling operations equipment.

The amount of PM10 and PM2.5 emission is calculated using the equation for bulldozing of overburden material provided in Table 11.9-1 of the EPA's AP-42. This equation estimates PM10 and PM 2.5 emissions in pounds per hour per vehicle, as follows:

$$= \frac{0.75 * 1.0 (s)^{1.5}}{(M)^{1.4}}$$

Where:

s = material silt content (%)

M = material moisture content (%)

1.4 and 1.5 = empiricle constants

0.75 = scaling factor to 10 um sized particles (PM10)

0.105 = scaling factor to 2.5 um sized particles (PM2.5)

Site-specific data:

material silt content, % =	9.2	[AP-42, Table 13.2.4-1, clay/dirt soil type]
material moisture content, % =	14.0	[AP-42, Table 13.2.4-1, clay/dirt soil type]
operation hours per year =	4,545	[client data]
number of dozers =	2	[client data]
number of compactors =	2	[client data]
number of loaders=	1	[client data]

Using the site-specific data as shown above, the PM10

$$[(0.75 * 1.0 * (\text{silt content, \%})^{1.5}) / (\text{moisture content, \%})^{1.4}] * (\text{operation hours/year}) * (\text{pieces of equipment, = total}) * (1 \text{ ton} / 2,000 \text{ lb})$$

$$= \frac{0.75 * 1.0 * (9.2)^{1.5}}{(14.0)^{1.4}} \quad \times \quad \frac{(4,545 * 5)}{2000}$$

$$= \quad \quad \quad \mathbf{5.9 \text{ tons filterable PM10 from working face filling operations equipment}}$$

Using the site-specific data as shown above, the PM2.5

$$[(0.105 * 1.0 * (\text{silt content, \%})^{1.5}) / (\text{moisture content, \%})^{1.4}] * (\text{operation hours/year}) * (\text{pieces of equipment, = total}) * (1 \text{ ton} / 2,000 \text{ lb})$$

$$= \frac{0.105 * 1.0 * (9.2)^{1.5}}{(14.0)^{1.4}} \quad \times \quad \frac{(4,545 * 5)}{2000}$$

$$= \quad \quad \quad \mathbf{0.8 \text{ tons filterable PM2.5 from working face filling operations equipment}}$$

B. Estimate of PM10 (dust) emissions from loading and unloading daily cover material.

The amount of PM10 emission is calculated using the emission factors for topsoil removal by scraper and scraper unloading, 0.058 lb. and 0.04 lb. dust per ton cover material respectively, as provided in Table 11.9-4 of the EPA's AP-42. Assume these factors represent both PM10 and PM 2.5 emissions.

These factors estimate dust emissions in pounds per the total amount of cover material used during the year, as follows:

$$= (0.058*W) + (0.04*W)$$

Where:

W = tons of cover material used

Site-specific data:

volume of cover material used, c.y. = 24,600 [client data]

The volume is converted to tons of cover material using an assumed density of 120 pound per cubic foot for soil as follows:

$$\text{Tons} = \text{volume (c.y.)} * (120 \text{ lb/ft}^3) * (27 \text{ ft}^3/\text{c.y.}) * (1 \text{ ton}/2,000 \text{ lb})$$

$$= 39,852 \text{ tons}$$

Using the site-specific data shown above, the PM10 and PM2.5 emissions are

$$= ([0.04 \text{ lb PM/ton} + 0.058 \text{ lb PM/ton}] * \text{tons cover material}) * [1 \text{ ton}/2,000 \text{ lb}]$$

$$= \frac{(0.058 + 0.04) * 131,798}{(2000)}$$

$$= \begin{matrix} \mathbf{2.0 \text{ tons filterable PM10 from unloading cover material}} \\ \mathbf{2.0 \text{ tons filterable PM2.5 from unloading cover material}} \end{matrix}$$

C. Estimate of PM10 (dust) emissions from hauling daily cover material.

The amount of PM10 emission is calculated using Equation 2 in Section 13.2.2 of the EPA's AP-42 (updated November 2006).

The equation estimates dust emissions in pounds per vehicle mile traveled (lb/VMT), with further calculation of total vehicle miles travelled and conversion from pounds to tons, as follows:

$$= k * (s/12)^a * (W/3)^b \quad \times \quad \frac{(365-p) * (1-R)}{365} \quad \times \quad \frac{(\text{Dist} * \text{Trips} * \text{Days})}{2,000 \text{ lb/ton}}$$

Where:

k, a, and b = Empiricle constants given by AP-42 (Table 13.2.2-2)

s = silt content (%)

W = vehicle weight, tons

p = number of days with at least 0.01 in. of precipitation per year

R = percent of time while operating water application vehicle (%)

Dist = distance (miles) from borrow area to working face

Trips = estimated number of loads (one way) per day x 2 (due to return trip to borrow area)

Days = number of working days per year

Site-specific data:

k, (lb/VMT) PM2.5 =	0.15	[AP-42, Table 13.2.2-2]
k, (lb/VMT) PM10 =	1.5	[AP-42, Table 13.2.2-2]
a =	0.9	[AP-42, Table 13.2.2-2]
b =	0.45	[AP-42, Table 13.2.2-2]
material silt content, % =	6.4	[AP-42, Table 13.2.2-1, Landfills]
mean vehicle weight, tons =	60.0	[estimated weight, manufacturer's info]
days per yr w/ 0.01 in. precipitation =	130	[per AP-42 Figure 13.2.2-1]
		[client data, 2 hours per day
R (%) =	25	operation of water truck]
driving distance, mi =	0.25	[client data]
trips per day =	3	[client data]
number of working days per year =	365	

Using the site-specific data as shown above, the filterable PM10

$$\begin{aligned}
 &= k \cdot (s/12)^a \cdot (W/3)^b \cdot (((365-p) \cdot (1-\text{percent watered}))/365) \cdot (1 \text{ ton}/2,000\text{lb}) \\
 &\quad \cdot \text{driving distance from borrow area to working face} \cdot \text{number of loads} \cdot 2 \text{ (for return to borrow area)} \cdot \text{working days} \\
 &= 1.5 \cdot (6.4/12)^{0.9} \cdot (60/3)^{0.45} \quad \times \quad \frac{(365-130)(1-0.25)}{365} \quad \times \quad \frac{(0.25 \cdot 4 \cdot 2 \cdot 365)}{(2000)} \\
 &= \quad \quad \quad \mathbf{0.4} \quad \quad \quad \mathbf{\text{tons filterable PM10 from hauling cover material}}
 \end{aligned}$$

Using the site-specific data as shown above, the filterable PM 2.5

$$\begin{aligned}
 &= k \cdot (s/12)^a \cdot (W/3)^b \cdot (((365-p) \cdot (1-\text{percent watered}))/365) \cdot (1 \text{ ton}/2,000\text{lb}) \\
 &\quad \cdot \text{driving distance from borrow area to working face} \cdot \text{number of loads} \cdot 2 \text{ (for return to borrow area)} \\
 &= 0.15 \cdot (6.4/12)^{0.9} \cdot (60/3)^{0.45} \quad \times \quad \frac{(365-130)(1-0.25)}{365} \quad \times \quad \frac{(0.25 \cdot 4 \cdot 2 \cdot 365)}{(2000)} \\
 &= \quad \quad \quad \mathbf{0.0} \quad \quad \quad \mathbf{\text{tons filterable PM2.5 from hauling cover material}}
 \end{aligned}$$

D. Totals

The total estimated filterable PM10 (dust) emission from landfiing activities is thus:

$$\begin{aligned}
 &= (\text{total from working face operations}) + (\text{total from loading/unloading daily cover material}) \\
 &\quad + (\text{total from hauling daily cover material}) \\
 &= (5.9 + 2.0+0.4) \\
 &= \quad \quad \quad \mathbf{8.3 \text{ Total tons filterable PM10 from landfilling activities}} \\
 &= 45.5 \text{ lbs/day PM10 from landfill activities}
 \end{aligned}$$

2008 Emission Statement
Millersville Landfill and Resource Recovery Facility

Calculated by: J. M. Demko
Checked by: J.G. Roth

The total estimated filterable PM2.5 (dust) emission from landfiing activities is thus:

$$= (\text{total from working face operations}) + (\text{total from loading/unloading daily cover material}) \\ + (\text{total from hauling daily cover material})$$

$$= 0.8+2.0+0.0$$

= **2.8 Total tons filterable PM2.5 from landfilling activities**

= 15.3 lbs/day PM10 from landfill activities

Table 3
2008 Air Toxic Emissions
Millersville Landfill and Resource Recovery Facility

User Inputs:

LFG generation flowrate (cfm) from LandGEM =
 Flare operational hours during year =
 LFG flowrate (cfm) collected, measured at flare =
 Average methane content of LFG collected, measured at flare =
 Flare Destruction Efficiency =

Calculations:

1,261 Annual methane generation (m3/yr) = 9.385E+06
 8,760 Annual LFG generation (m³/yr)
 1,185 assuming 50% methane content = 1.88E+07
 52.2% LFG Collection Efficiency = 98.11%
 99.91%

Pollutant	Mol. Wt. (g/gmol)	Concentration (ppmv)	Source (AP-42, Site Data)	Air Toxic Generation (m ³ /yr)	Air Toxic Generation (kg/yr)	Air Toxic Emissions								Total Air Toxic Emissions		
						Fugitive Emissions (lb/yr)	Flare Emissions (lb/yr)	Fugitive Emissions (tpy)	Flare Emissions (tpy)	Fugitive Emissions (lb/hr)	Flare Emissions (lb/hr)	Fugitive Emissions (lb/day)	Flare Emissions (lb/day)	tpy	lbs/day	lbs/hr
Acrylonitrile	53.06	0.036	WIAC	0.6	1.3	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.00	0.0	0.00
Benzene	78.11	0.818	site data	14.0	44.6	1.9	0.1	0.001	0.000	0.0002	0.0000	0.0	0.0	0.0	0.0	0.00
Benzyl chloride	126.6	0.04	site data	0.7	3.5	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.0	0.0	0.00
Bromoform	252.73	1.9	site data	32.5	335.4	13.9	0.7	0.007	0.000	0.0016	0.0001	0.0	0.0	0.0	0.0	0.00
Carbon disulfide	76.13	0.05	site data	0.9	2.7	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0	0.0	0.0
Carbon tetrachloride	153.84	0.03	site data	0.5	3.2	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.0	0.0	0.00
Carbonyl sulfide	60.07	0.08504	site data	1.5	3.6	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0	0.0	0.0
Chlorine	35.45	9.43	WIAC	161.1	233.5	9.7	0.0	0.005	0.000	0.0011	0.0000	0.0	0.0	0.0	0.0	0.0
Chlorobenzene	112.56	0.049	site data	0.8	3.9	0.2	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0	0.0	0.0
Chloroform	119.38	0.02	site data	0.3	1.7	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.0	0.0	0.0
1,4-Dichlorobenzene(P)	147	0.03	site data	0.5	3.1	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0	0.0	0.0
1,2-Dichloropropane (propylene dichloride)	112.99	0.03	site data	0.5	2.4	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0	0.0	0.0
Ethyl benzene	106.17	4.28	site data	73.1	317.4	13.2	0.6	0.007	0.000	0.0015	0.0001	0.0	0.0	0.0	0.0	0.0
Ethyl chloride (chloroethane)	64.52	0.464	site data	7.9	20.9	0.9	0.0	0.000	0.000	0.0001	0.0000	0.0	0.0	0.00	0.0	0.000
Ethylene dibromide (1,2-dibromoethane)	187.88	0.03	site data	0.5	3.9	0.2	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.000	0.0	0
Ethylene dichloride (1,2-dichloroethane)	98.96	0.032	site data	0.5	2.2	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0	0.0	0
Ethylidene dichloride (1,1 Dichloroethane)	98.97	0.808	site data	13.8	55.9	2.3	0.1	0.001	0.000	0.0003	0.0000	0.0	0.0	0.0	0.0	0.0
Hexachlorobutadiene	260.76	0.05	site data	0.9	9.1	0.4	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.00	0.0	0.000
n-Hexane	86.18	2.324	WIAC	39.7	139.9	5.8	0.3	0.003	0.000	0.0007	0.0000	0.0	0.0	0.0	0.0	0.0
Hydrochloric acid	---	---	site data	---	---	---	245.3	---	0.120	---	0.0280	---	---	0.1	0.7	0.0
Hydrogen sulfide	34.06	7.8	site data	133.2	185.6	7.7	---	0.004	---	0.0009	---	0.0	---	0.00	0.0	0.0
Mercury & compounds	200.61	0.000292	AP-42	0.0	0.0	0.0	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.000	0.0	0.0000
Methyl chloride (Chloromethane)	50.49	0.05	site data	0.9	1.8	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.00	0.0	0.0
Methyl chloroform (1,1,1 Trichloroethane)	133.41	0.025	site data	0.4	2.3	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.00	0.0	0.0
Methyl isobutyl ketone (MIBK)	100.16	0.75	WIAC	12.8	52.5	2.2	0.1	0.001	0.000	0.0002	0.0000	0.0	0.0	0.00	0.0	0.0
Methylene chloride (Dichloromethane)	84.94	2.82	site data	48.2	167.3	7.0	0.3	0.003	0.000	0.0008	0.0000	0.0	0.0	0.00	0.0	0.0
Styrene	104.2	0.243	site data	4.2	17.7	0.7	0.0	0.000	0.000	0.0001	0.0000	0.0	0.0	0.00	0.0	0.0
1,1,2,2-Tetrachloroethane	167.85	0.03	site data	0.5	3.5	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.00	0.0	0.0
Tetrachloroethylene (Perchloroethylene)	165.83	1.17	site data	20.0	135.5	5.6	0.3	0.003	0.000	0.0006	0.0000	0.0	0.0	0.00	0.0	0.0
Toluene	92.14	31.6	site data	593.3	2,235.8	93.0	4.3	0.046	0.002	0.0106	0.0005	0.3	0.0	0	0	0
1,2,4-Trichlorobenzene	181.45	0.06	site data	1.0	7.6	0.3	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.00	0.0	0.0
1,1,2-Trichloroethane	133.4	0.03	site data	0.5	2.8	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.00	0.0	0.0
Trichloroethylene (Trichloroethene)	131.38	0.499	site data	8.5	45.8	1.9	0.1	0.001	0.000	0.0002	0.0000	0.0	0.0	0.00	0.0	0.0
Vinyl chloride	62.5	1.52	site data	26.0	66.4	2.8	0.1	0.001	0.000	0.0003	0.0000	0.0	0.0	0.00	0.0	0.0
Vinylidene chloride (1,1-Dichloroethene)	96.94	0.03	site data	0.5	2.0	0.1	0.0	0.000	0.000	0.0000	0.0000	0.0	0.0	0.00	0.0	0.0
Xylenes	106.17	16.582	WIAC	283.2	1,229.8	51.1	2.4	0.026	0.001	0.0058	0.0003	0.1	0.0	0.0	0	0
o-Xylene	106.17	1.28	site data	21.9	94.9	3.9	0.2	0.002	0.000	0.0005	0.0000	0.0	0.0	0.0	0	0
m,p-Xylene	106.17	11.1	site data	189.6	823.3	34.2	1.6	0.017	0.001	0.0039	0.0002	0.1	0.0	0.0	0	0

- Notes:
- Hydrochloric acid emissions are estimated using stack test results from Kilkelly Environmental Associates, which showed HCL emissions of 0.028 lb/hr.
 - There are no chlorine flare emissions, as chlorine is converted to HCL during combustion.
 - Site specific data was from laboratory testing completed April 2004.
 - Default values are based on values from "Waste Industry Application Coalition Comparison of Recent Landfill Gas Analyses with Historic AP-42 Values" dated January 2001

Table 4
2008 Air Toxic Emissions
Millersville Landfill and Resource Recovery Facility
Anne Arundel County, Maryland

User Inputs for Horizontal Grinder Engine:

Gallons used [gal/yr]	5,602.7
Heating value of diesel [Btu/gal]	142,000
Hours of operation [hrs/yr]	485
Days of operation [days/yr]	312

Pollutant	Emission Factor lb/MMBtu	Source (AP-42, Site Data)	Total Air Toxic Emissions		
			(lb/day)	(lb/hr)	(tpy)
			Acetaldehyde	2.52E-05	AP-42
Acrolein	7.88E-06	AP-42	0.0	0.000	0.00
Benzene	7.76E-04	AP-42	0.0	0.00	0.00
Formaldehyde	7.89E-05	AP-42	0.0	0.000	0.00
Naphthalene	1.30E-04	AP-42	0.0	0.000	0.00
Toluene	2.81E-04	AP-42	0.0	0.000	0.00
Xylenes	1.93E-04	AP-42	0.0	0.000	0.00

**Table 5 - 2008
Annual Emissions
Millersville Landfill
Billable Toxic Air Pollutants**

Total Methane Generation (m3/yr) = 9,384,987
 LFG Collection Efficiency (%) = 98.11%
 Flare Destruction Efficiency = 99.91%
 Hours operation = 8,760

HAP	MW	*Conc. (ppbv)	Billable TAP Emissions								
			Fugitive Emissions (lb/yr)	Flare Emissions (lb/yr)	Fugitive Emissions (lb/day)	Flare Emissions (lb/day)	Fugitive Emissions (lb/hr)	Flare Emissions (lb/hr)	Fugitive Emissions (tons/yr)	Flare Emissions (tons/yr)	
carbon disulfide (1)	76.13	50	0.1	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00
carbonyl sulfide (2)	60.07	85.04	0.1	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00
chlorine (2)	35.45	9430	9.7	0.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
hydrochloric acid (2)	n/a	n/a	0	245.3	0.00	0.67	0.00	0.03	0.00	0.00	0.12
methyl chloroform (1)	133.41	25	0.1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
methylene chloride (1)	84.94	2820	7.0	0.33	0.02	0.00	0.00	0.00	0.00	0.00	0.00
perchloroethylene (1)	165.83	1170	5.6	0.26	0.02	0.00	0.00	0.00	0.00	0.00	0.00

1. Concentration, in parts per billion by volume, from the results of site LFG testing, conducted in April 22, 2004
2. Concentration, in parts per billion by volume, from AP-42.
3. There are no chlorine emissions from flaring, as chlorine is converted to HCL during combustion.
4. Hydrochloric acid emissions are estimated using stack test results from Kilkelly Environmental Associates, which showed HCL emissions of 0.028 lb/hr.